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Review

# A Review of Orbital Angular Momentum Vortex Beams Generation: From Traditional Methods to Metasurfaces

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**Abstract:** In this paper, we review the generation of vortex beams carrying orbital angular momentum in the microwave domain. We firstly present the theory of Laguerre–Gaussian beams where it is demonstrated that they carry such type of momentum. We further provide an overview of the classical methods used to generate orbital angular momentum vortex beams, which rely on two main methods; plane wave to vortex wave conversion and direct generation using radiating antennas. Then, we present recent progress in the physics of metasurfaces devoted to the generation of vortex beams with a discussion about reflective and transmissive metasurfaces for plane wave to vortex wave conversion as well as methods to reduce the intrinsic divergence characteristics of vortex beams. Finally, we conclude on this rapidly developing research field.

**Keywords:** vortex beams; orbital angular momentum; microwave antennas; metasurfaces

## 1. Introduction

From Maxwell's theory, it is well known that electromagnetic (EM) waves carry both linear momentum and angular momentum. The angular momentum is composed of two parts: spin angular momentum (SAM) corresponding to the polarization of the EM wave and orbital angular momentum (OAM) associated to the spatial distribution of the EM wave.

SAM of an EM wave has been recognized for a long time and it carries  $\pm \hbar$  per photon. However, OAM has only attracted valuable attention since 1992 when Allen et al. [1] showed that Laguerre–Gaussian (LG) beams possess an orbital angular momentum of  $l\hbar$  per photon, where  $l$  is an integer and refers to the topological charge (order) of the OAM mode, i.e., the number of phase twists around the vortex. In 1994, Allen et al. further discussed the relationship between non-paraxial beams and angular momentum since LG beams are not exact solutions of the full Maxwell's theory that are only the solutions of the paraxial wave equation [2]. Under the condition of non-paraxial approximation, theoretical calculation results show that OAM still depends on the topological charge  $l$ . As long as the beams contain spiral phase, they will carry an OAM mode. It provides a simpler way to generate OAM, that is, vortex beams can be excited with a plane wave. While the phase of a plane wave is constant on the wavefront, the phase  $\alpha$  of an OAM wave undergoes a linear variation along the angular coordinate with  $\alpha = l\varphi$ . The field hence varies as  $e^{-jl\varphi} f_l(r) \cdot e^{-jkz}$ , where  $k$  is the wave vector,  $z$  is the propagation axis and  $f_l(r)$  represents the field variation along the radial coordinate.

Early studies in optical regime concerning the interaction of OAM with matter raised applications in optical tweezers [3,4], optical drive of micro-machines [5], atoms trapping and guiding [6,7], microscopy [8], and photon entanglement [9]. In the radiofrequency (RF) domain, OAM has been firstly proposed to improve spectral efficiency in radio communications by creating multiple propagation

sub-channels corresponding to the twisting degree of the EM wave [10–14]. Other possible applications of OAM include object identification [15] and radars [16–20].

It is common to generate OAM beams in the optical domain, especially when the programmable spatial light modulator (SLM) is available [21]. Existing optical devices can also provide mature schemes to manipulate OAM beams such as combination, splitting, collimation, concentration, and detection [22–25]. However, in RF and microwave domains, the wavelength is much longer than in optics, and therefore it is difficult to manipulate microwave OAM beams, such as beam combining and splitting, since coaxial transmission cannot be easily ensured. Therefore, for applications in microwave domain, the OAM wave generation method is very important to ensure optimal performances of the whole system. The main goals of this review work is to present an overview of the OAM beam generation through the use of metasurfaces. The paper is structured as follows: Section 1 presents a brief introduction on OAM and Section 2 focuses on Laguerre–Gaussian (LG) beams carrying OAM. In Section 3, we present the mostly used classical methods to generate vortex waves and Section 4 deals with the use of metasurfaces for OAM beam generation. Finally, Section 5 serves as a general conclusion.

## 2. Laguerre–Gaussian Beams Carrying OAM

In theory, any field in free space can be described by a continuous spectrum of cylindrical waves which is characterized by Laguerre polynomials [26]. Different expressions strictly satisfy the orthogonal relation. Beams propagating in the  $-z$ -direction in free space can be expressed as:

$$E(r, \varphi, z) = u(r, \varphi, z)e^{jkz} \tag{1}$$

where  $u(r, \varphi, z)$  is the amplitude of beams in cylindrical coordinates,  $k$  is the wave number in free space. The space EM waves also satisfy the Helmholtz equation:

$$(\nabla^2 + k^2)E(r, \varphi, z) = 0 \tag{2}$$

The substitution of Equation (1) into the scalar wave Equation (2) gives:

$$\frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial u}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 u}{\partial \varphi^2} + \frac{\partial^2 u}{\partial z^2} + 2jk \frac{\partial u}{\partial z} = 0 \tag{3}$$

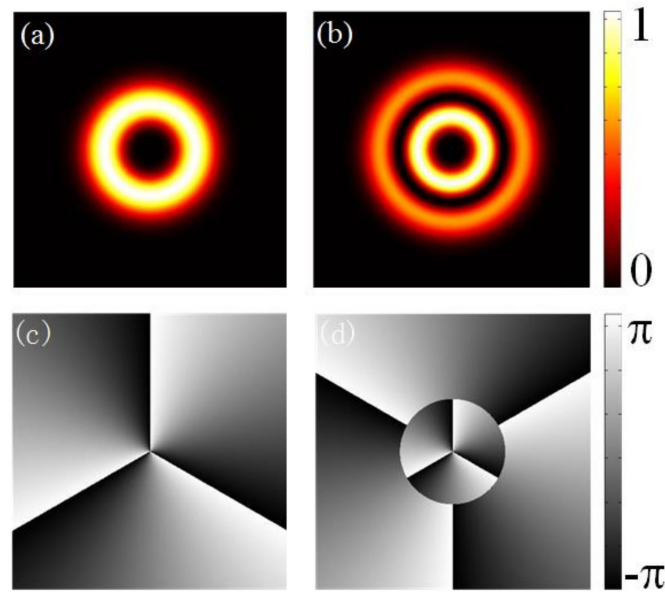
The electric field amplitude in the  $z$ -direction varies much slowly compared to the transverse field in the beam. Therefore, the paraxial wave equation is derived when the second derivative in the  $z$ -direction is ignored. Then, the cylindrically symmetric solutions Laguerre–Gaussian beams are given by [1]:

$$LG_{pl} = \sqrt{\frac{2p!}{\pi(p+|l|)!}} \frac{1}{w(z)} \left[ \frac{r\sqrt{2}}{w(z)} \right]^{|l|} \exp\left[ \frac{-r^2}{w^2(z)} \right] \times L_p^{|l|} \left[ \frac{2r^2}{w^2(z)} \right] \exp(jl\varphi) \times \exp\left[ \frac{jk_0 r^2 z}{2(z^2 + z_R^2)} \right] \times \exp\left[ j(2p + |l| + 1) \tan^{-1} \left( \frac{z}{z_R} \right) \right] \tag{4}$$

where  $w(z)$  is the radius of the beams,  $z_R$  is the Rayleigh range.  $l$  and  $p$  are angular index and radial index, respectively.  $L_p^{|l|}(x)$  is the associated Laguerre polynomial, which is derived from:

$$L_p^{|l|}(x) = (-1)^{|l|} \frac{d^{|l|}}{dx^{|l|}} L_{p+|l|}(x) \tag{5}$$

Different LG beams are determined by different number of  $l$  and  $p$ . All LG beams constitute a set of complete orthogonal basis vectors that can represent any spatial beams. The amplitude and phase distributions with different  $l$  and  $p$  values are shown in Figure 1. The radius of the ring-shaped beam will diffract when  $l$  increases, while the parameter  $p$  will lead to a change in the number of rings.



**Figure 1.** Illustration of Laguerre–Gaussian beams. (a,b) Amplitude, (c,d) phase distribution of the beams with  $l = 1, p = 0$  (a,c) and  $l = 3, p = 1$  (b,d).

In 1992, Allen et al. pointed out that the LG beams have a well-defined orbital angular momentum where the spatial phase factor  $e^{-jl\varphi}$  corresponds to the orbital angular momentum. The angular momentum density can be expressed as:

$$M = \varepsilon_0 r \times (E \times B) \tag{6}$$

where  $\varepsilon_0$  is the permittivity,  $E$  and  $B$  represent the electric field and magnetic field, respectively. In classical mechanics and atomic physics, angular momentum can be decomposed into SAM and OAM. Therefore, the total angular momentum is:

$$J = L + S = \varepsilon_0 \int r \times (E \times B) dr \tag{7}$$

where  $L$  represents OAM and  $S$  represents SAM. For a linear polarized wave, the time averaged angular momentum density is obtained when applied to LG beams expression:

$$M = -\frac{l}{w(z)} \frac{z}{r} |u|^2 r + \frac{r}{\sqrt{\frac{2p!}{\pi(p+|l|)!}}} \left[ \frac{z^2}{(z^2 + z_R^2)} - 1 \right] |u|^2 \varphi + \frac{l}{w(z)} |u|^2 z \tag{8}$$

The first two terms of the expression are symmetrical about the axis which are related to SAM. Therefore, the integration the angular momentum  $J$  will only remain the third term which is related to OAM. Similarly, for circularly polarized wave, the angular momentum power of  $z$  component is:

$$M_z = \frac{l}{w(z)} |u|^2 + \frac{\sigma_z r}{2w(z)} \frac{\partial |u|^2}{\partial r} \tag{9}$$

where  $\sigma_z = \pm 1$  for left handed and right handed circularly polarized (LHCP and RHCP) beams. As such, orbital angular momentum is theoretically demonstrated in the LG beams.

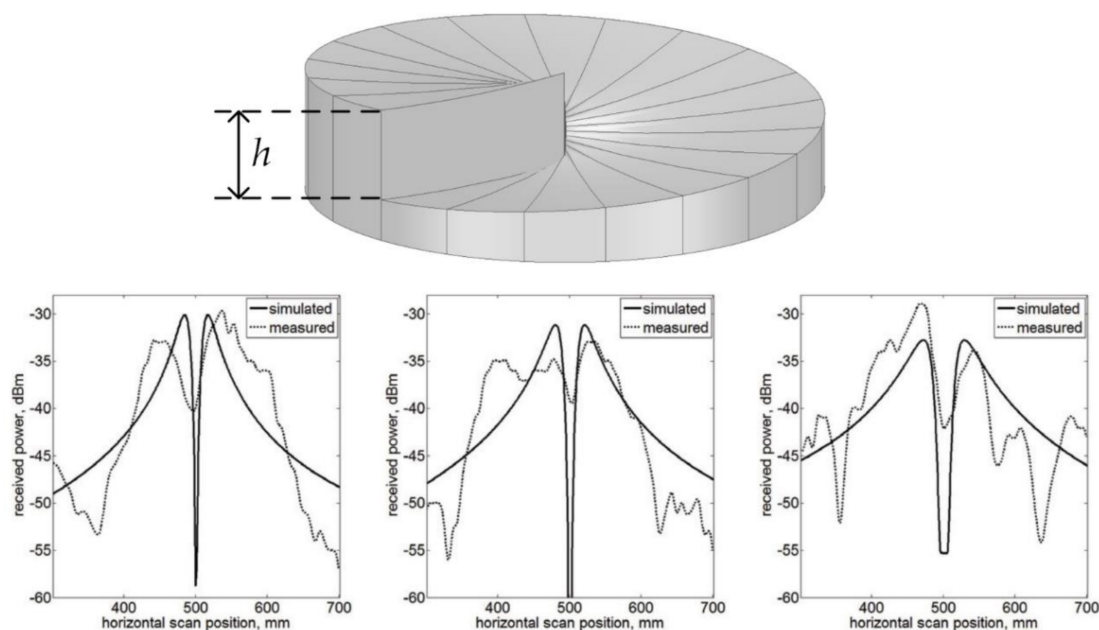
### 3. Classical Methods for Generating OAM Waves in RF Domain

The first RF OAM wave generation from microwave antennas was presented by Thidé et al. in 2007 [27]. Since then, the study of EM waves carrying OAM in the RF and microwave domains

is constantly growing. Classically, in the radio domain, two main families of structures have been proposed to generate OAM waves. The first one consists in transforming a plane wave and can be achieved by using spiral phase plates [28,29], flat drilled phase plates [30,31], spiral [32] or twisted reflectors [11,33], and holography with a diffraction grating structure. In the second one, the OAM wave is directly generated using circular phased radiator arrays [10,34–39].

### 3.1. Spiral Phase Plate (SPP)

A spiral phase profile is obtained when a plane wave passes through a system of varying phase. Spiral phase plates (SPPs) come from the optical frequency region and are generally made of a material with constant refractive index and a radially varying thickness, as illustrated in Figure 2. Usually, the higher the topological charge is desired, the bigger is the thickness difference in the SPP. The advantages of SPP reside in small OAM beam divergence and low attenuation. The main disadvantages of the SPPs are that they are not operational for low-frequency signal transmission and since the design is fixed, they cannot provide simultaneous generation of several different OAM topological charges. The studies presented in References [28,29] have been performed in the millimeter wave frequency band at 86 and 60 GHz, respectively. Two different phase plates were designed in [28] and were made of polyethylene having a refractive index of 1.52 at millimeter-wave frequencies. One was utilized to generate the  $LG_0^1$  mode and the other one to generate the  $LG_0^2$  mode. The step heights of the phase plates were 6.7 mm and 13.4 mm respectively to give a single and a double wavelength step at 86 GHz. The main characteristic of a vortex OAM beam which is the null of energy at the center of the radiated beam (doughnut shaped radiation pattern) can be clearly observed in the results presented in Figure 2.



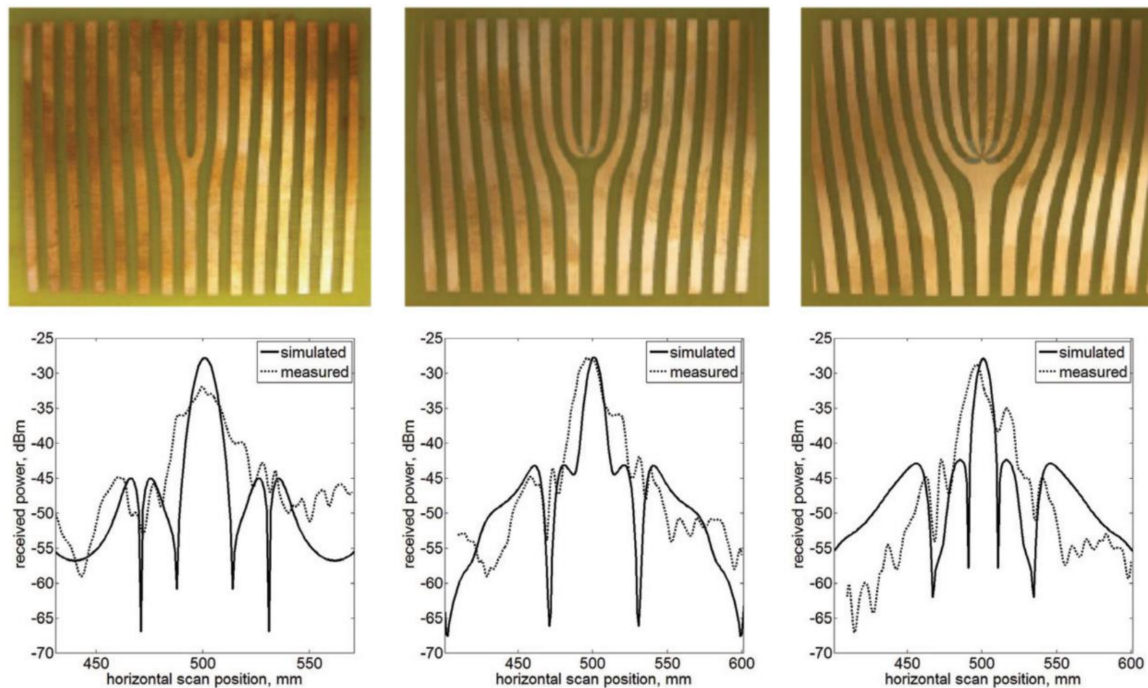
**Figure 2.** Schematic design of a spiral phase plate and results obtained at 60 GHz in [29].

### 3.2. Flat Drilled Phase Plate

SPP can also be designed by drilling holes in a constant height dielectric bulk material in order to engineer the required spiral phase profile through effective permittivity tailoring. This kind of SPP can be referred as flat drilled phase plate. Such work has been realized at 32 GHz to generate OAM waves with topological charge  $l = -1$  [30,31]. A horn antenna, commonly used in the microwave range for its high directivity and low sidelobes level, was used as the incident wave source to illuminate the phase plate, compared to a Gaussian beam generally used in optics.

### 3.3. Diffraction Grating

Diffraction grating is an optical structure composed of either parallel slits or parallel lines to operate in transmission or reflection mode, respectively. In OAM field, it is used as a hologram. When illuminated by a light beam, the structure diffracts the light into several beams in different directions and an interference pattern (hologram) is obtained by the interference between the incident and the diffracted beams. It is then possible to record the hologram between the two beams and then to use it to generate one beam from the other [40]. Such hologram has been applied in Ref. [29] to generate OAM vortex waves at 60 GHz (Figure 3) by illuminating the grating structure with a Gaussian beam transmitter.

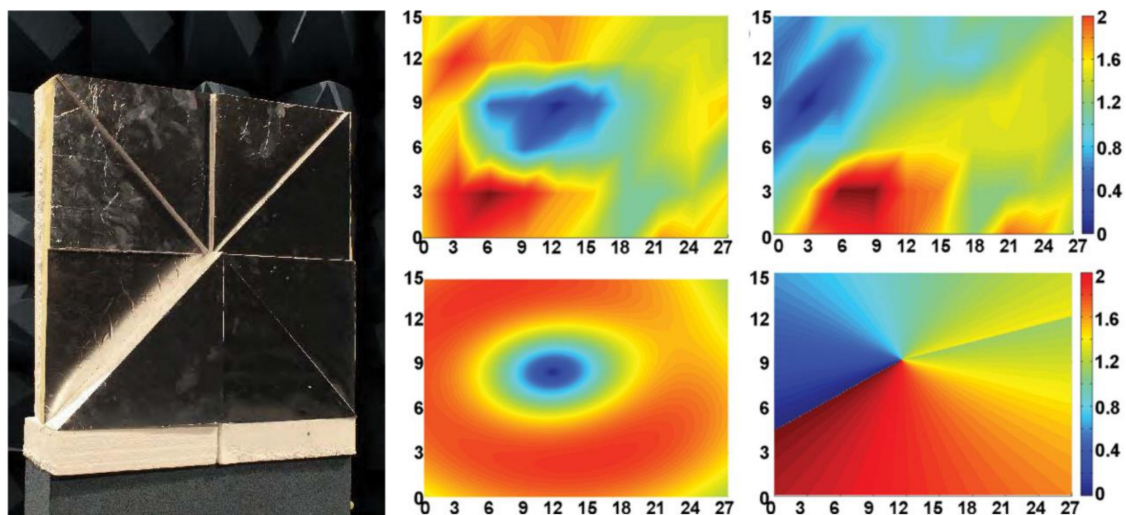


**Figure 3.** Designs of several holograms for orbital angular momentum (OAM) vortex wave generation and the obtained radiation patterns in far-field at 60 GHz [29].

The main elements of holographic masks are observable in the fork-grating dislocation (Figure 3), where the plane input wave is transformed through this zone. The shape and behavior of fork-grating is controlled by the topological charge  $l$ . Conversely to the spiral phase plate or flat drilled phase plate, and by observing the patterns in Figure 3, the hologram not only produces OAM vortex waves but also a Gaussian beam at boresight ( $0^\circ$ ) due to the illuminating wave. The output signal carries OAM on the sides of the centered Gaussian beam.

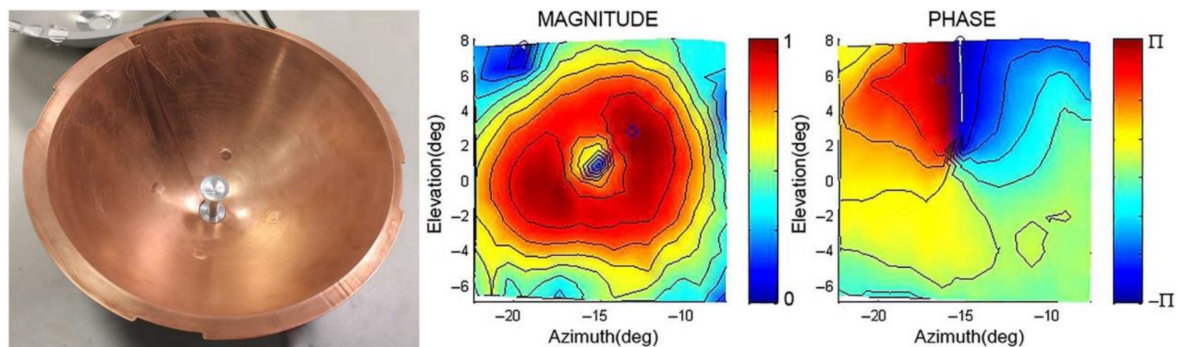
### 3.4. Spiral and Twisted Reflectors

The spiral reflector proposed in [32] was made from styrofoam blocks, covered with an electrically conductive and reflective surface and was illuminated by a seven-element Yagi-Uda antenna intended for 2.4–2.5 GHz wireless local area network (WLAN) communications (Figure 4). The radio beam is reflected off the discrete eight-step staircase phase mask representing a discrete approximation of a non-focusing spiral reflector designed for a total  $2\pi$  phase shift spiral.



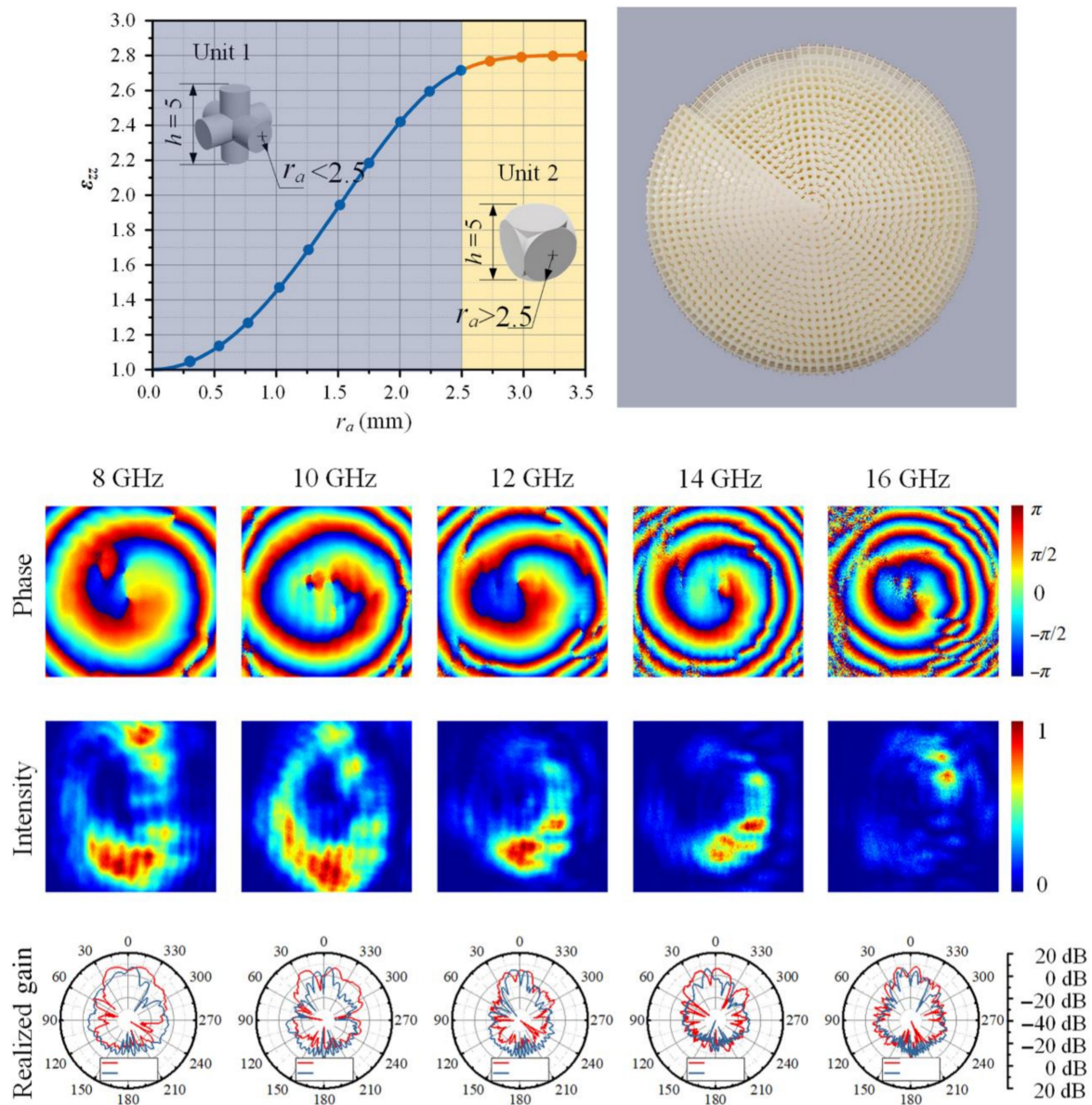
**Figure 4.** Photography of the spiral reflector and the near electric-field intensity and phase patterns measured (top) and simulated (bottom) at 2.4 GHz [32].

In [11,33], a helicoidal parabolic (twisted reflector) antenna was used to generate a vortex wave with a feeding source located at the focal point (Figure 5). The twisted reflector converts the field generated by the feeding source into a helical beam with a topological charge  $l$  that depends on the height of the step of the twisted reflector.



**Figure 5.** Photography of the twisted reflector and the electric-field magnitude and phase patterns measured in the far-field at 17.2 GHz [33].

Such helicoidal parabolic reflector was recently flattened by the use of the transformation optics (TO) mathematical concept [41,42] and metamaterial structures. In [43,44], a spatial TO-based OAM generation method was proposed to design a flattened perfect electric conductor (PEC) backed three-dimensional (3D) printed cylindrically shaped dielectric structure so as to mimic a twisted reflector (Figure 6). The TO-based generation method allows to transform a certain zone above the helicoidal parabolic antenna into an oblate cylindrical space. This transformation led to a medium characterized by a permittivity distribution varying from 1 to 2.8, allowing a 3D printing of the device. By transmitting through the calculated oblate cylindrical space, a plane wave emitted from the feeding source is transformed into a vortex beam after its reflection from the grounded planar surface rather than from the helicoidal parabolic reflector. The all-dielectric OAM generation device is capable of maintaining performance over a broad frequency range since all-dielectric non-resonant materials are used in the design, as illustrated in Figure 6.



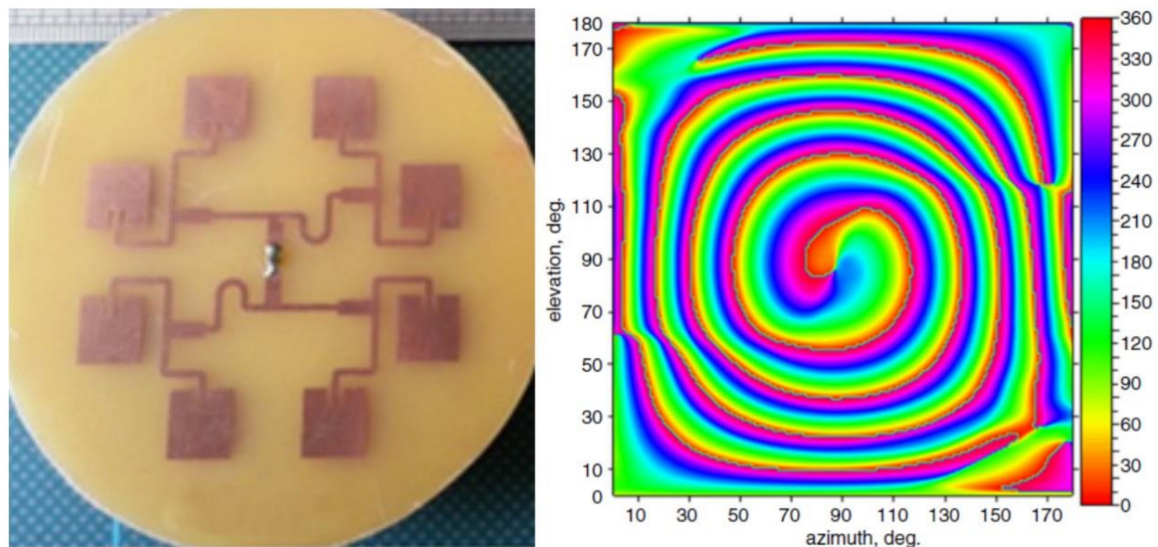
**Figure 6.** Three dimensional (3D) printed dielectric structure mimicking placed on a flat perfect electrical conductor (PEC) surface mimicking a helicoidal parabolic reflector. The near-field and far-field results show a broadband frequency operation from 8 GHz to 16 GHz, thanks to the use of non-resonant dielectric structures [44].

### 3.5. Circular Phased Arrays

The last approach concerns the direct generation of OAM beams through the application of uniform circular arrays (UCA) of radiating elements with a particular feeding system that allows specifying the required phase shift for each radiator corresponding to the generation of the selected OAM state. The number of radiators in the array has an additional influence on the OAM antenna, since it determines the largest OAM mode that can be generated. In 2007, Thidé et al. numerically designed the first microwave OAM radiator using a circular distributed radiator array [27]. UCA allows generating several different OAM modes by changing the phase shift from the feeding system and to shift the OAM state without changing the antenna configuration. However, the main disadvantage of UCA is the high divergence feeding system complexity. Later, other works have been presented on the generation of OAM vortex waves based on UCA [34–39]. In [34], instead of feeding all the



radiators at the same time with a particular phase-shift between the elements, the radiators are fed sequentially with the same amplitude and phase. The first experimental results on UCA were presented in [36], where eight radiators were used in the array to generate mode  $l = -1$  (Figure 7). Other types of radiating elements have been further used in the circular arrays, such as horn antennas [38] and single-arm spiral antennas [39].



**Figure 7.** Photography of the first experimental prototype of a phased antenna array for OAM vortex wave generation and its measured phase pattern [36].

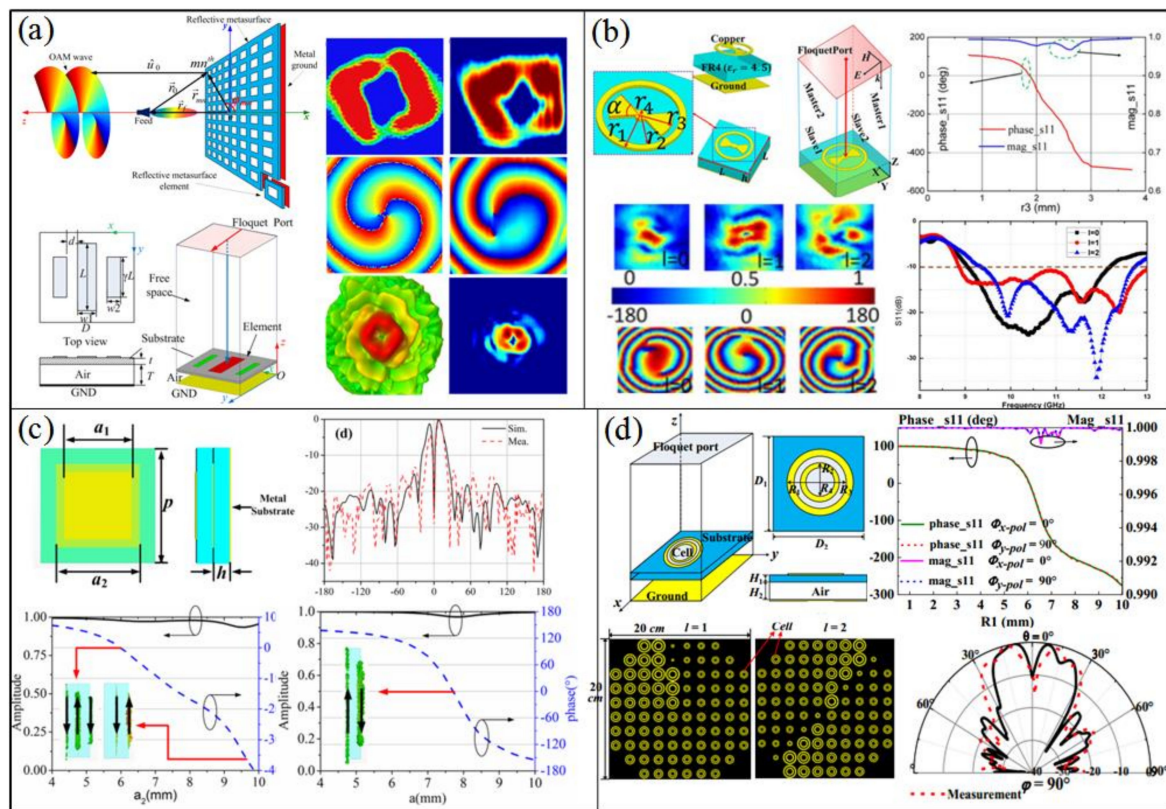
Since the vortex beam diverges rapidly along propagation direction, different solutions have been proposed to reduce the divergence angle and increase the gain. For instance, a Fabry–Perot cavity in which a highly-reflective surface served as the superstrate, was numerically evaluated to generate a high gain vortex wave [45]. Afterwards, electromagnetic band-gap (EBG) superstrate was used to achieve high gain OAM vortex waves [46]. Lenses based on the use of metasurfaces [47,48] and all-dielectric materials [49,50] have further been applied to reduce beam divergence of OAM vortex waves generated by phased antenna arrays.

#### 4. Metasurfaces for OAM Beam Generation

The conventional methods to generate vortex beams in microwave region have been discussed in the previous section. In the case of the circular phased array antennas, a complex feeding system should be implemented to accomplish spiral phase distribution with consistent power delivery. Besides, it needs more antenna elements when the number of OAM modes increases which will lead to a feed network more complex in the design process. Phase plates and reflectors are bulky structures that are usually not suitable for implementation in modern communications systems. Recently, metasurfaces (MS) have drawn much attention due to the unique ability of arbitrary wavefront control, such as amplitude, phase and polarization state of EM waves. Compared to metamaterials, metasurfaces are two-dimensional surface arrays with the advantages of low profile, light weight and ease of fabrication. For OAM generation, we classify metasurfaces into two main categories: reflective and transmissive. For reflective MS, amplitude attenuation is generally negligible and only a single layer of structure is generally required to achieve the coverage of the spiral phase. In contrast, transmissive MS for OAM generation are in most cases composed of several layers to achieve the required  $2\pi$  phase shift needed for plane wave to vortex wave conversion and attention has to be paid to losses in the multi-layer structure.

### 4.1. Reflective Metasurfaces

In Reference [51], a propagation phase reflective metasurface is designed to effectively generate single vortex beam with orbital angular momentum in the radiofrequency domain, as shown in Figure 8a. The unit cell consists of three patch dipoles. By controlling the length of the three patches and the distance between them, the reflected wave has a continuous reflection phase range of more than  $2\pi$ . Based on the proposed unit cell, a reflective metasurface with  $20 \times 20$  elements is designed to generate vortex beam carrying an OAM mode with topological charge  $l = 2$  at 5.8 GHz. A metasurface composed of ring-surrounded bowtie patch resonators is proposed in [52]. The structure is inspired by the bowtie antenna which has wideband characteristics (Figure 8b). A linear phase variation is obtained when varying the radius of the bowtie patch under TM wave incidence. Several metasurfaces have been designed to generate OAM modes with  $l = 0, 1, 2$  over about 3 GHz bandwidth. Single layer resonant structures are easy to fabricate, but the phase varies drastically at the resonant frequency, resulting usually in a narrow bandwidth.

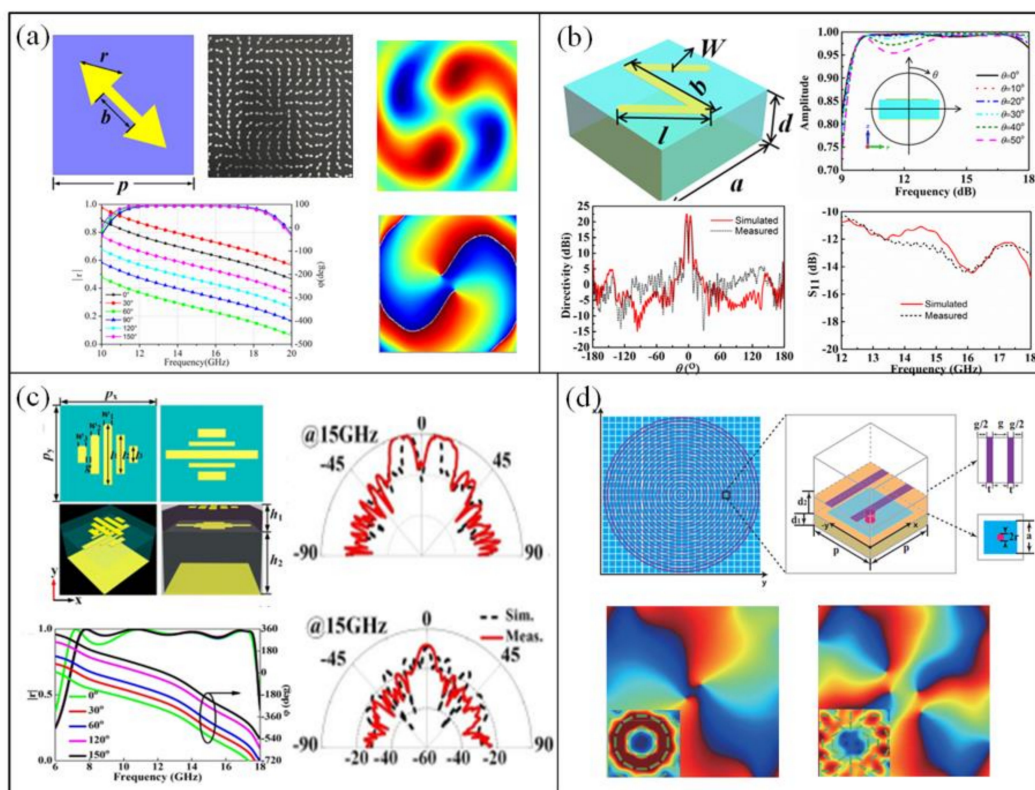


**Figure 8.** Reflective OAM metasurfaces based on propagation phase. (a) Linear polarized (LP) vortex beams [51]. (b) Wideband linear polarized vortex beams [52]. (c) Double-layered unit for wideband vortex beams [53]. (d) Polarization insensitivity OAM metasurfaces [54].

In Reference [53], double-layered elements are used to design MS for the generation of broadband vortex beams. The unit cell is composed of two square patches separated by a dielectric substrate instead of only one patch in a single layer structure, as illustrated in Figure 8c. For one patch element, a strong magnetic resonance occurs between the patch and ground plane of the reflective MS, while for double-layered element, the magnetic resonance is due to the interaction between the two patches and the ground plane for low frequency and to the interaction between mainly the two patches for high frequency. Therefore, the phase response is more flat and the operational bandwidth is enhanced. The proposed metasurface generates vortex beams carrying an OAM mode  $l = 1$  in the 8.5 GHz–11.5 GHz frequency range. Due to limitation of unit cell topology, the metasurface in [51] and [52]

can only operate under single polarized incident waves. By properly designing the elementary cell pattern (Figure 8d), a polarization-insensitive OAM metasurface is proposed in [54]. Two concentric rings guarantee structural symmetry when introducing enough phase-shift range. The spiral phase distribution is realized by changing the radius of the inner and outer rings. A reflectarray-type prototype with  $l = 1$  is fabricated to demonstrate the design at 5.8 GHz.

The phase shift of the metasurfaces in [51–54] can be controlled not only through varying structure parameters to introduce propagation phase, but also through rotation of the orientation of the meta-atom to introduce geometric phase. Compared to propagation phase, geometric phase which is usually called Pancharatnam–Berry (PB) phase is easier to implement. When the unit cell is rotated, the emitted phase of the cross-polarized component will have a phase shift as twice as the rotated angle under circular polarized (CP) incident wave. Therefore, only single-sized unit cell is needed which has the ability to convert CP wave to its cross polarization rather than a plurality of different-sized unit cells [55–59]. Besides, the unit cells with different rotation angles have the same dispersion characteristics and hence, the bandwidth of the vortex beams are usually broad. In Reference [55], an ultra-broadband reflective metasurface based on PB phase to generate vortex beams is proposed. A double arrow-shaped metallic layer is applied to achieve perfect CP wave conversion (Figure 9a). The metasurface presents an efficiency of 75.76% to excite vortex beams with OAM mode  $l = 2$  in the 12 GHz–18 GHz frequency range. The N-shaped resonator based on PB phase is employed to achieve nearly 100% conversion efficiency in Reference [56]. The unit cell is suitable for broadband design which transmits 98% energy of incident CP wave to its cross-polarized wave (Figure 9b). Besides, when the incident angle varies from  $0^\circ$  to  $50^\circ$ , the conversion efficiency is higher than 90% in 8 GHz frequency bandwidth. The metasurface generates vortex beams with OAM mode  $l = 1$  from 12 GHz to 18 GHz. Similarly, the polarization conversion bandwidth can also be expanded with a double layer unit cell.



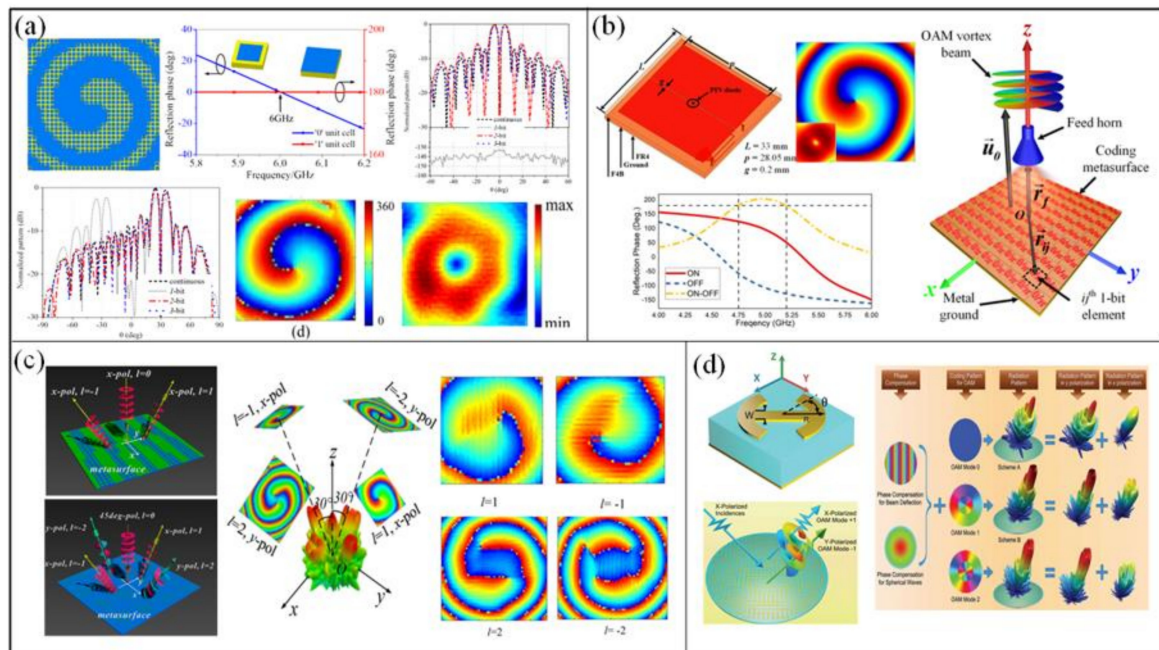
**Figure 9.** Reflective OAM metasurfaces based on geometric (PB) phase. (a) Double arrow-shaped metasurface [55]. (b) N-shaped resonator metasurface [56]. (c) Double-layered cross dipoles metasurface for a wideband vortex beams [57]. (d) OAM metasurface based on perfect electric conductor–perfect magnetic conductor (PEC-PMC) elements [60].

A dual-layer meta-atom that can manipulate phase shift independently for  $x$ - and  $y$ -polarized waves is proposed in Reference [57]. The unit cell consists of five symmetric parallel dipoles with different parameters in each layer, as shown in Figure 9c. The reflection phase can be controlled independently without much crosstalk by arranging the dual-layer orthogonally. It is much easy to achieve CP wave polarization conversion over large bandwidth. The bandwidth of the metasurface generating vortex beams with OAM mode  $l = 1$  ranges from 6.95 GHz to 18 GHz. A perfect electric conductor-perfect magnetic conductor (PEC-PMC) anisotropic metasurface for OAM generation is proposed in Reference [60] and is illustrated in Figure 9d. The top surface of the unit cell acts as a PEC surface which consists of two metal strips behaving like a parallel-plate waveguide. The  $x$ -polarized wave is totally reflected with an offset phase of  $\pi$ , while the  $y$ -polarized wave will transmit through it. The bottom surface acts as a PMC surface which is realized by the mushroom-like high-impedance surface. It reflects the  $y$ -polarized wave with zero phase shift. In this way, the unit can realize the perfect polarization conversion of CP wave. Two types of metasurface carrying an OAM mode  $l = 2$ , consisting of azimuthally continuous loops and azimuthally discontinuous loops, are designed based on the proposed unit cell. It can be observed that the continuous one shows smoother phase distribution than the discontinuous one.

A series of unit cells with continuous phase shift constitutes some difficulties in the design process. Though the introduction of PB phase can simplify the design, it can only operate under CP wave. Recently, digital metamaterials have been presented to create a new connection between the physical structure and digital information. The beams can carry specific information with only a few unit cells by digital coding. When the concept comes to the two-dimensional metasurface, the coding can be implemented by the reflected or transmitted phase and amplitude of the unit cells. The simplest one-bit code can be realized by the reflection phases  $0^\circ$  and  $180^\circ$ . A one-bit coding metasurface was proposed to generate vortex beams in Reference [61]. The elementary cell is composed of a metallic patch and a metallic ground plane printed on the two faces of a dielectric substrate. The reflection phase of two unit cells are  $0^\circ$  and  $180^\circ$ , respectively. The reduction of the coding number does not influence the divergence angle of main lobe, but the existence of quantization error will raise the side lobes. Besides, the one-bit quantization method does not have enough resolution to generate the vortex beam without any additional compensation in the normal direction for plane wave incidence. However, if other phase profiles, such as the spherical wave phase, are introduced into the vortex beam, then the quantization error will show pseudo-random distribution. Such a coding metasurface with OAM mode  $l = 1$  was fabricated to demonstrate the effectiveness of the concept at 6 GHz and is shown in Figure 10a.

A tunable metasurface generating vortex beams with any OAM modes is proposed in Reference [62]. A positive intrinsic negative (PIN) diode is utilized as a switch between the two rectangular patches constituting the unit cell of the metasurface, as presented in Figure 10b. The two states "0" and "1" are realized by switching the PIN diode, controlled by direct current (DC) voltage, to ON and OFF states. Therefore, any OAM mode can be realized by switching the states of each unit cells judiciously on the metasurface. In Reference [63], a multiple OAM vortex beams is generated by one-bit coding metasurface. Combining the phase distribution of vortex beam with the phase distribution required for beam steering functionality, the incident energy can be redirected into desired directions. Due to the periodic variation of the phase,  $0^\circ$  phase is also regarded as  $2\pi$  phase. In other words, the variation of phase from 0 to  $\pi$  also means variation of phase from  $2\pi$  to  $\pi$ . Therefore, for one-bit coding beam steering, a vortex beam will reflect into two opposite directions under normally incident plane wave. The cross-dipole structure is utilized to manipulate  $x$ -polarized and  $y$ -polarized wave, respectively (Figure 10c). Then, by combining the coding of two orthogonal directions, the incident waves are simultaneously converted to vortex beams with  $l = \pm 1$  and  $l = \pm 2$  in different directions at 8.5 GHz. Another method to design coding OAM metasurface based on polarization bit was proposed in Reference [64]. The unit cell can cover  $2\pi$  reflection phase for linearly polarized waves by adjusting each parameter (Figure 10d). Besides, when rotating the structure by  $\pm 45^\circ$ , the polarization state of the

reflected wave is converted to its cross-polarized component. The metasurface is divided into two regions: inner region and outer region. Each region determines whether to convert the polarizations of incident beam or not and modulate the OAM modes into the reflected beam. Under illuminating  $x$ -polarized wave, two vortex beams carrying OAM modes  $l = 1$  and  $l = 2$  in the  $x$ - and  $y$ - polarized component can be clearly observed at 15 GHz, respectively.

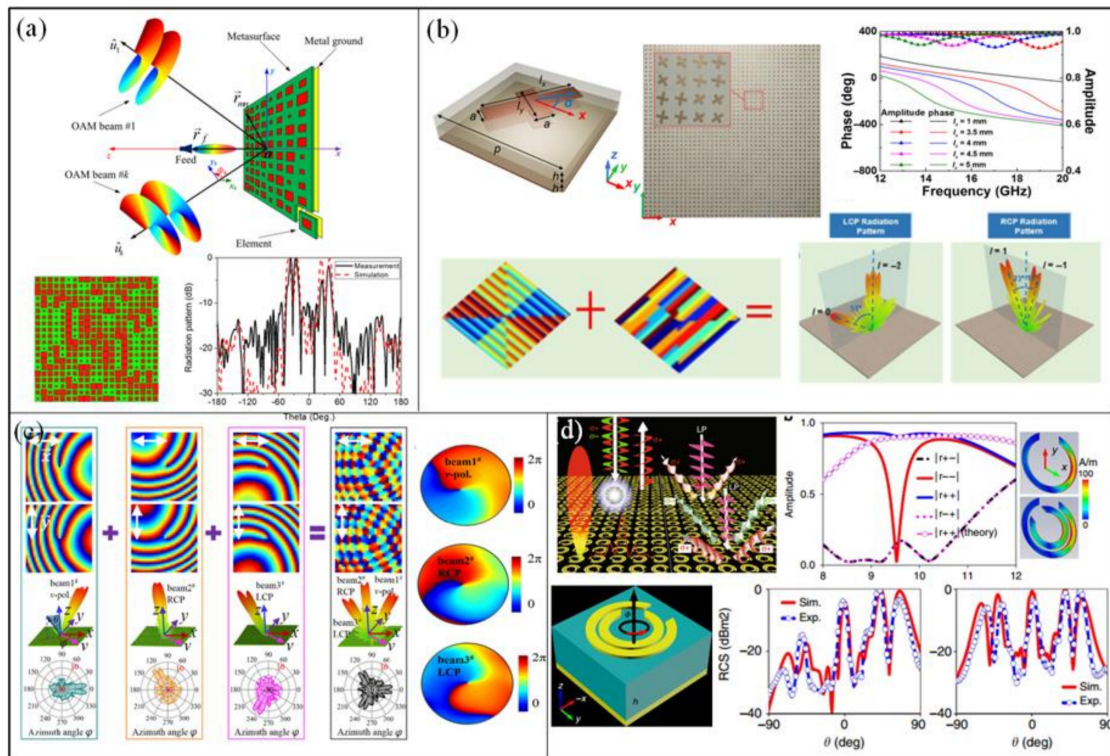


**Figure 10.** Digital coding OAM reflective metasurface. (a) One-bit passive OAM metasurface [61]. (b) One-bit active OAM metasurface [62]. (c) One-bit dual polarization OAM metasurface [63]. (d) Five-bit multi-polarization OAM metasurface [64].

To enhance the information capacity of a metasurface, a single linear polarization reflective metasurface generating multiple vortex beams with different OAM modes in different directions was proposed in Reference [65]. The unit cell consists of only one patch element, as shown in Figure 11a. The reflected phase has a continuous change when the length of patch is increased or decreased. When vortex beams with different OAM modes are excited in the same direction, the mode order will be the sum of them. Therefore, different vortex beams can only be generated in different directions. Besides, interference may occur if the beams are close to each other. By compensating the phase of different OAM modes and diffraction direction, the metasurface generates two vortex beams with  $l = 2$  in opposite propagation directions ( $\theta = \pm 30^\circ$ ). The operational frequency range of the metasurface spans from 5.5 GHz to 6.5 GHz.

Another way to expand the channel capacity is to control the polarization of wave freely. For linear polarized wave, it can be easily realized by a unit cell that can control phase shift for  $x$ - and  $y$ -polarized waves independently. However, for CP wave, it is hard to control LHCP and RHCP independently when only geometric phase is utilized because they are constrained to be conjugate values in the electric field form. In other words, vortex beams will have opposite mode number for LHCP and RHCP. To overcome the limitation, a metasurface merges propagation phase and geometric phase together in Reference [66]. It can be demonstrated that the analytical solutions for reflective dual-helicity decoupled wavefront control contains the  $x$ -polarized reflection phase  $\phi_x$ , the  $y$ -polarized reflection phase  $\phi_y$ , and the rotation angle  $\alpha$ . Besides,  $\phi_x$  and  $\phi_y$  have a phase difference of  $\pi$ . The unit cell consists of dual-layer cross dipole and a ground plane (Figure 11b). In order to simplify the design, the unit cells are transformed into digital coding cells. The phase coverage is discretized by  $45^\circ$  gradient into 64 unit cells for two CP waves and each polarization has eight states. A complex coding

distribution was realized according to the demand. The metasurface generating the vortex beam with OAM mode  $l = 1$  in  $xoz$  plane under LHCP wave and two pencil beams in the  $yoz$  plane for RHCP wave at 16 GHz was fabricated to demonstrate the theory. In Reference [67], independent control of polarizations, beam numbers, OAM modes and orientations were proposed by phase compensation. The unit cell is composed of two orthogonal I-shaped dipoles able to control the phase shift of  $x$ - and  $y$ -polarized waves independently. To verify the proposed approach, a metasurface generating triple vortex beams was designed; one has the mode  $l = -1$  for the linear polarized (LP) wave and mode  $l = +1$  for the RHCP and LHCP waves (Figure 11c).



**Figure 11.** Multiplexed OAM reflective metasurfaces. (a) Single linear polarization reflective metasurface to generate multiple vortex beams [65]. (b) Circular polarized (CP) wave decoupling to achieve multiplexed vortex beams [66]. (c) Full polarization multi-beams [67]. (d) A decoupling method to generate dual CP vortex beams at different frequencies [68].

A decoupled method for CP wave is proposed in Reference [68] which excites vortex beams under single CP wave. The unit cell consists of two split ring resonators (SRRs) which are twisted to each other by  $45^\circ$ , as shown in Figure 11d. Both SRRs can introduce PB phase with 100% efficiency under illuminating CP wave. Moreover, they exhibit symmetric and asymmetric modes parallel and perpendicular to the symmetry axis. According to Jones matrix, the in-phase constructive interference for co-polarized CP wave and out-of-phase destructive interference for cross-polarized CP wave are realized when the phase difference between two CP waves is  $\Delta\phi = -90^\circ$  and the twist angle of two SRRs is  $45^\circ$ . A metasurface able to generate two RHCP vortex beams at 9.5 GHz and four LHCP vortex beams at 10.5 GHz was designed.

#### 4.2. Transmissive Metasurfaces

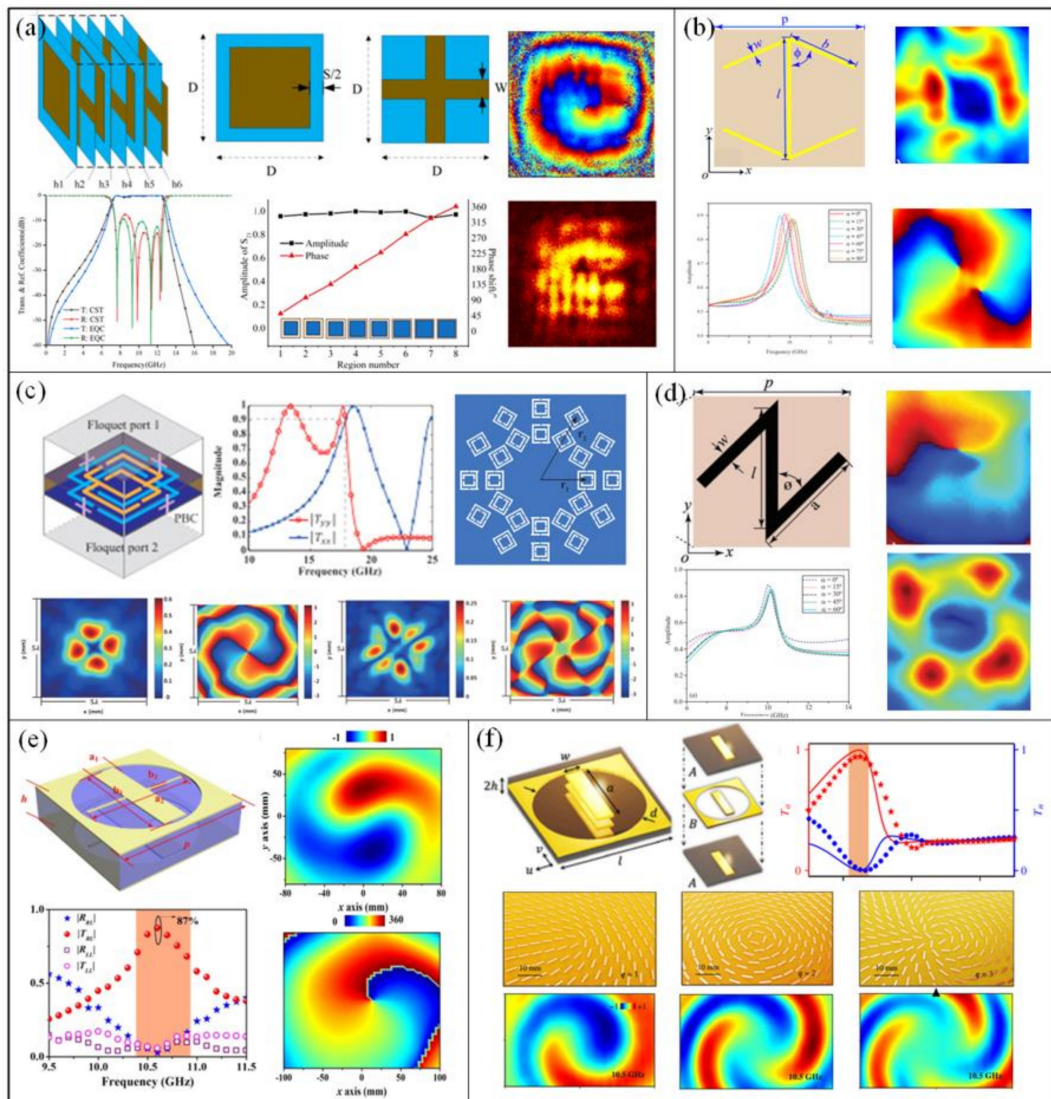
For transmissive OAM metasurfaces, generation efficiency needs to be considered since there is no ground plane to reflect all energy. It has been demonstrated that only 25% efficiency can be achieved in a single layer structure due to no excitation of magnetic resonance [69,70]. The design of a high efficiency transmissive metasurface is therefore a challenging problem that merits to be considered.

A unit cell consisting of a cylindrical dielectric resonator and a metallic rod to manipulate the EM wavefront was proposed in Reference [71]. The metallic rod provides the necessary broadband electric polarization, and the cylindrical dielectric resonator provides the necessary broadband magnetic polarization. By tuning the unit parameters,  $2\pi$  phase shift can be covered with high transmission magnitude. According to the concept of gradient phase discontinuity, a vortex beam carrying an OAM mode  $l = 1$  can be generated by the flat spiral gradient phase with high efficiency at in the 8 GHz–9.8 GHz frequency band. However, to have strong electric and magnetic resonances, the length of the cylindrical rod must not be too short. The overall thickness of the metasurface is 10 mm ( $0.3\lambda_0$ ).

Miniaturized element frequency selective surfaces (MEFSS) were proposed to generate high efficiency vortex beams in Reference [72]. The elementary cell is composed of four layers of patches and three layers of wire grids alternately separated by dielectric substrates (Figure 12a). The patches are considered as capacitors while the wire grids are considered as inductors. The cascading distance can be effectively reduced by the strong coupling of the two kind of components. By tuning the size of patches, eight unit cells can be obtained with a transmission phase gradient of  $45^\circ$  and nearly 100% efficiency at 10.6 GHz. Even though the amplitude is non-uniform, the efficiency of vortex beams with  $l = 1$  exceeds 60% in the 10 GHz–11.3 GHz frequency band. The overall thickness is only  $0.15\lambda_0$ .

A subwavelength scatterer based on photon spin Hall effect (PSHE) to generate high efficiency OAM waves was proposed in Reference [73]. The proposed unit cell consists of two double-headed arrows printed on the top and bottom of the dielectric substrate (Figure 12b). By introducing the magnetic resonance, the unit cell can effectively convert CP wave to its cross-polarized component in transmission. The conversion efficiency attains 84.6% at 10 GHz. However, when the unit cell is rotated to introduce PB phase, the amplitude of cross-polarized component cannot be kept constant, resulting in a reduction of the efficiency of the vortex beams excitation. The metasurface generating vortex beams with  $l = 2$  presents an efficiency of 45% with a thickness of  $0.05\lambda_0$ . In Ref. [74], a unit cell consisting of complementary split ring resonators (CSRRs) for full phase control in a 0.8 mm ( $0.05\lambda_0$ ) thick metasurface was presented (Figure 12c). The proposed unit cell transmits a circularly polarized wave to its cross-polarized component with a high efficiency of 81%. The calculated conversion efficiency of OAM beams with  $l = 1$  in the transmitted wave is up to 81.8% while the total transmission efficiency is only 15.2% and it becomes lower for higher modes. This is mainly due to the fact that compared to the whole metasurface, the scatterers are too few to satisfy the periodicity along  $x$ - and  $y$ -directions.

In Reference [75], the efficiency was enhanced by dual-layer Z-shaped metallic patterns shown in Figure 12d. The unit cell has nearly the same polarization conversion efficiency as two double-headed arrow unit, but the amplitude is more stable when it is rotated. A transmission efficiency of 55% is achieved for the same OAM mode  $l = 2$ . An ultrathin unit cell was proposed in Reference [76] to generate high efficiency vortex beams. The unit consists of a cross-bar structure with positive permittivity and holey metallic ring resonator with negative permittivity on both sides of a dielectric substrate (Figure 12e). The transmission amplitude and phase can be controlled independently by the length of the cross bar. When the transmission phase in the two orthogonal directions has a phase difference of  $\pi$ , 95% conversion efficiency of the cross-polarized component can be obtained at 10.6 GHz. The maximum excitation efficiency reaches 87% for OAM mode  $l = 1$  and the overall thickness of the metasurface is only  $0.07\lambda_0$ . A nearly 100% efficiency photonic spin hall effect (PSHE) PB meta-atom named as ABA structure, with A and B representing two metal layers, was proposed in Reference [70]. The unit cell is composed of three metallic layers. Layer A is realized by an anisotropic resonator of rectangular patch while Layer B is realized by a holey metallic film coupled with a metallic bar (Figure 12f). The conversion efficiency could reach 91% at 10.5 GHz. Three vortex beam carrying OAM modes 1, 2, 3 were constructed by the ABA units in different metasurfaces of thickness  $0.125\lambda_0$ , respectively.

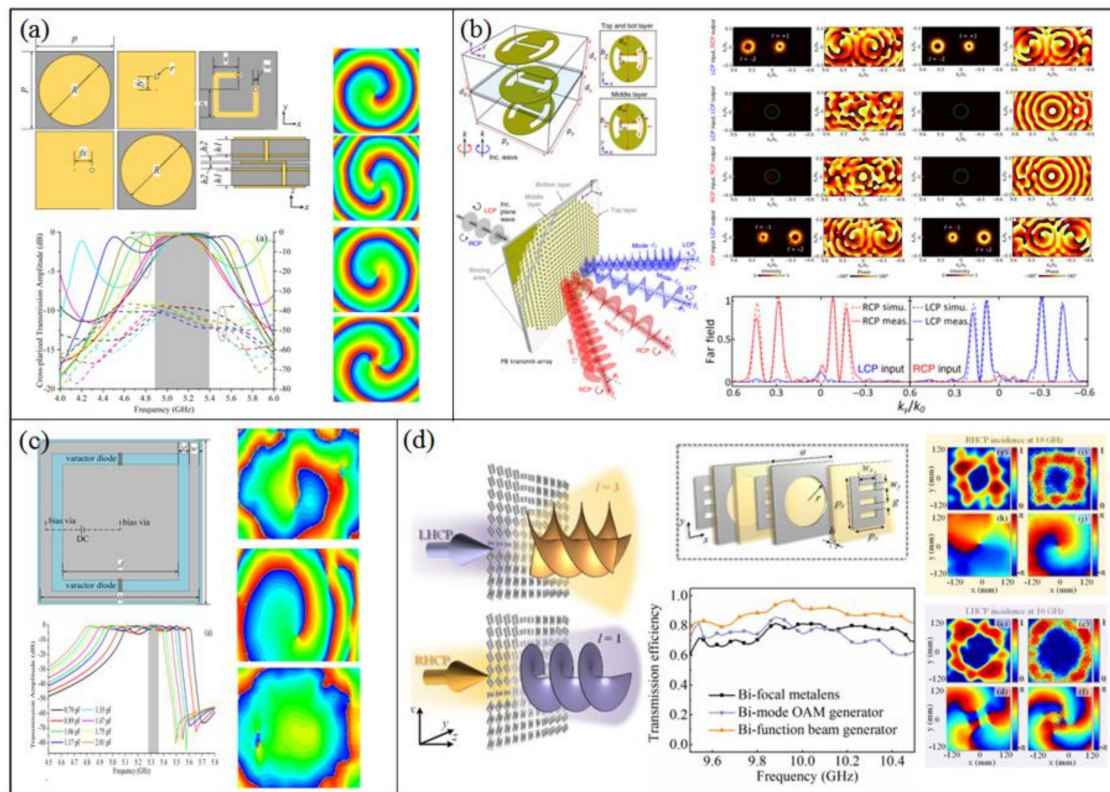


**Figure 12.** Transmissive OAM metasurfaces. (a) OAM metasurfaces based on MEFSS [72]. (b) OAM metasurfaces based on photon spin Hall effect (PSHE) unit of two double-headed arrows [73]. (c) OAM metasurfaces based on complementary split ring resonators [74]. (d) OAM metasurfaces based on PSHE unit of Z-shaped cell [75]. (e) OAM metasurfaces based on cross bar and holey metallic ring resonator [76]. (f) OAM metasurfaces based on ABA structure [70].

The polarization state of EM wave can be set as a convenient switch to alter the different output wavefronts generated by bi-functional meta-devices. In Reference [77], the authors designed a multilayer unit cell that was inspired from the patch antenna (Figure 13a). The unit cell has five metallic layers and four dielectric layers. The top patch can couple the linear-polarized wave into the guided mode in the stripline structure, and the bottom patch decouples the guided wave into its cross-polarized component. Different transmission phase distributions are introduced by different length of the stripline with low transmission losses. Two metasurfaces of thickness  $0.074\lambda_0$  with different OAM modes of 1 and 2 were designed through the transmission phase steps of  $45^\circ$  and  $90^\circ$ , respectively. Due to the asymmetry of the polarization conversion, the metasurfaces were able to excite two opposite modes simultaneously, +1 and +2 modes for  $x$ -polarized wave and  $-1$  and  $-2$  modes for  $y$ -polarized wave at 5.14 GHz. An active metasurface to separately generate vortex beams carrying different modes is proposed in Reference [78] (Figure 13c). The unit cell consists of a patch and a metallic loop. Two varactor diodes are placed in the gaps between them which is controlled by a DC bias voltage with a low transmission loss. When the reverse voltage bias varies from 0 V to 30 V,



$2\pi$  phase coverage can be easily obtained. Three different orders of OAM modes  $l = +1, l = -1$  and  $l = 0$  are separately excited at 5.35 GHz. The efficiency of the three modes are about 45%.

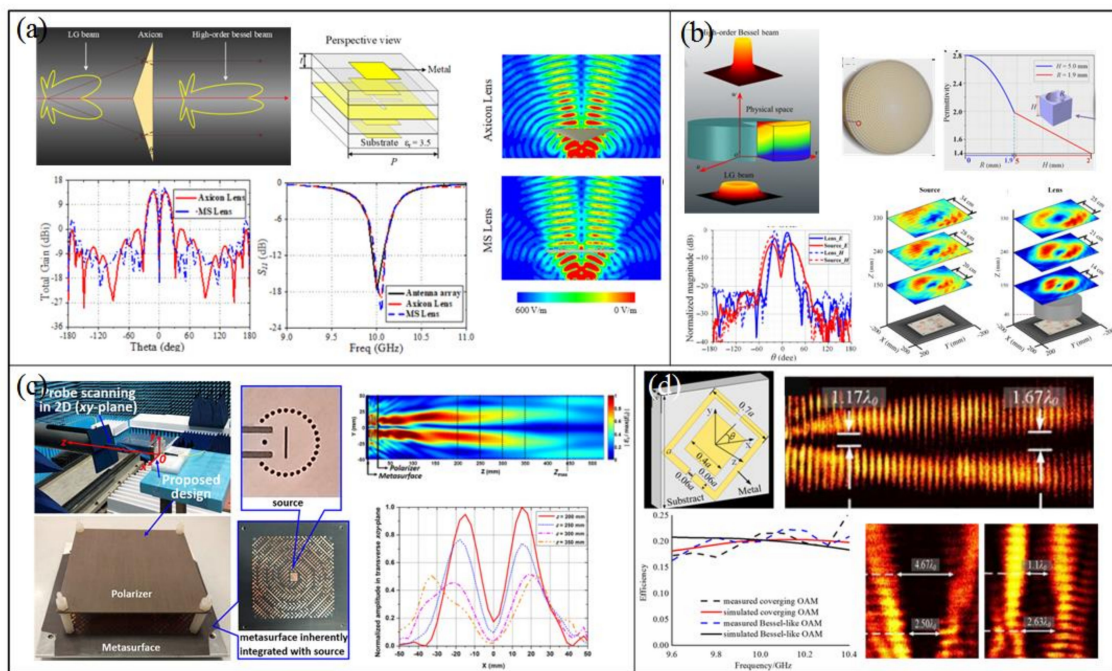


**Figure 13.** (a) OAM metasurfaces based on multi-layer CP conversion unit [77]. (b) Vortex beams multiplexing based on CP wave [79]. (c) Multiple OAM modes by active metasurface [78]. (d) CP wave decoupled OAM metasurface [80].

In Reference [79], a multiplexed CP vortex beam generator is proposed by overlapping the phase masks of a harmonic spatial light modulator and spiral phase plates. The unit cell cascades three anisotropic impedance surfaces with custom-designed anisotropy to achieve high efficiency of circular polarization conversion, as shown in Figure 13b. A single vortex-beam PB transmitarray ( $l = 1$ ) was designed which could bend the wave towards the direction of a particular diffraction mode with a high purity. The efficiency of the generated vortex beams was 88% at 29.4 GHz and over 50% in a non-narrow bandwidth of 17%. A dual vortex beam transmitarray was designed by incorporating spiral phase profiles into a harmonic-response spatial light modulator with tailored intensity. When the structure is illuminated by circularly polarized incident wave, two vortex beams with OAM modes  $l = 1$  and  $l = -2$  are excited in different diffraction directions. The dual OAM beams metasurface achieve 71% efficiency at 29.4 GHz and over 50% in a frequency bandwidth of 13%. In Reference [80], the authors proposed a mechanism for producing distinct OAM modes in orthogonal circular polarized (CP) transmitted fields, which breakthrough the inherent symmetric restriction between orthogonal CP waves (Figure 13d). The vortex beam carrying an OAM with mode  $l = 1$  was generated in the cross-polarized output field under RHCP illumination, while the OAM with mode  $l = 3$  is produced through cross-polarization under LHCP illumination. The polarization state of incident wave acts as the important role for altering the distinct OAM modes, and hence dual mode vortex beams have been generated conveniently and effectively.

### 4.3. Divergence Reduction of OAM Vortex Beams

Vortex waves present divergence characteristics in propagation, which become worse when the OAM topological order increases and also when propagation distance increases. It might limit the practical applications of vortex beams for long distance communications or transmitting systems. A common solution is to converge the vortex beam. However, the limitation of this method is that it can only focus the beam to a point close to the metasurface rather than propagating over a long distance. In Reference [47], a flat metalens was proposed to collimate the vortex waves (Figure 14a). The converging lens system is excited by an OAM beam generator composed of a conventional circular patch antenna array source consisting of eight patches with the same phase shift between each of the neighboring elements. The metasurface is placed at a distance  $2\lambda$  above the antenna source to compensate the phase of vortex beams. The divergence characteristics of vortex beams are obviously improved as they transmit through the metalens around 10 GHz frequency. Meanwhile, the propagation directivity and gain are also enhanced from 9 dBi to 15 dBi. The transmission efficiency is over 75% and reaches 88.14% at 10 GHz. Moreover, the purity of OAM mode  $l = 1$  is degraded by only 1%. In Reference [50], a broadband all-dielectric 3D-printed cylindrical collimating lens was proposed to solve the divergence characteristics drawback of vortex beams (Figure 14b). The design comes from the transformation optics concept. By solving the transformation equations of Laguerre–Gaussian (LG) to high-order Bessel (HOB) beam, the permittivity distribution of the metamaterial medium is obtained. The equivalent permittivity was varied by considering air holes in a bulk dielectric medium. The permittivity decreases when the radius of the cylindrical cavity increases. The divergence angle and diameter of the vortex beams can be greatly reduced through the metamaterial medium. The frequency bandwidth was about 8 GHz around 10 GHz operating frequency thanks to the use of all-dielectric non-resonant unit cells.



**Figure 14.** Non-diffraction OAM metasurfaces and metamaterials. (a) A collimating metalens [47]. (b) A collimating all-dielectric metamaterial medium [50]. (c) A metasurface to generate non-diffraction vortex beams and convert the polarization of the LP wave [81]. (d) A converging OAM metasurface and a non-diffractioning OAM metasurface [82].

The integration of the vortex beam excitation and the non-diffraction function can be realized by phase compensation. In Reference [81], a reflective metasurface was presented to generate a non-diffractive Bessel beam carrying OAM modes. The system consists of three parts; a circular cavity

backed substrate-integrated waveguide (SIW) source, a polarizer, and the metasurface, as shown in Figure 14c. The metasurface converts the linear polarized incident wave to its cross-polarized component carrying non-diffraction vortex beams at 40.25 GHz. In Reference [82], the authors proposed a general scheme to optimize the divergence constraints of vortex beams (Figure 14d). Firstly, the converging phase distribution has been imposed into the vortex beam, which can effectively focus the OAM with required mode into preset plane, where the radius of converged vortex beam in focal plane can be decreased by nearly four times. This focused OAM can be effectively applied in communication systems, where the propagation distance is specifically fixed. On the other hand, the spatial phase profile of Bessel beam has been added into a vortex beam, which can produce quasi-non-diffractive OAM beam within a long propagation distance. It can be obviously seen that the combination with different functional wavefronts can effectively optimize the divergent property of traditional vortex beam, and realize OAM carrying new and useful properties.

## 5. Conclusions

In this paper, a review has been made on the generation of OAM vortex beams in the microwave domain. In a first step, we have presented the theory of Laguerre–Gaussian beams, where it is shown that they possess a well-defined orbital angular momentum. We have also reviewed the main classical methods used to generate such beams. They mainly include structures such as phase plates, reflectors and diffraction gratings for transforming plane waves to vortex waves and antenna arrays for direct radiation of electromagnetic waves carrying OAM. More recently, metasurfaces have revolutionized the way of tailoring electromagnetic properties and functionalities through the engineering of subwavelength elements. In this context, metasurfaces, whether they operate in a reflection or transmission manner, have been applied to transform plane waves to vortex waves carrying OAM. Moreover, functionalities such as Bessel beam profile and converging lens profile have been combined with OAM phase profile to be integrated in a single metasurface in order to reduce the intrinsic divergence characteristics of OAM beams.

In the view of the implementation of metasurfaces for the generation of vortex waves carrying orbital angular momentum, practical applications in the area of wireless communications can be considered. OAM metasurfaces can indeed offer simple and low-cost systems, along with high efficiency and other combined functionalities such as lensing. However, efforts towards integrated illuminating sources still need to be done.

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